



De-Icing for More Efficient Renewable Energy

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Team 06-709 - ENGS 90 - 25W

Team Roles



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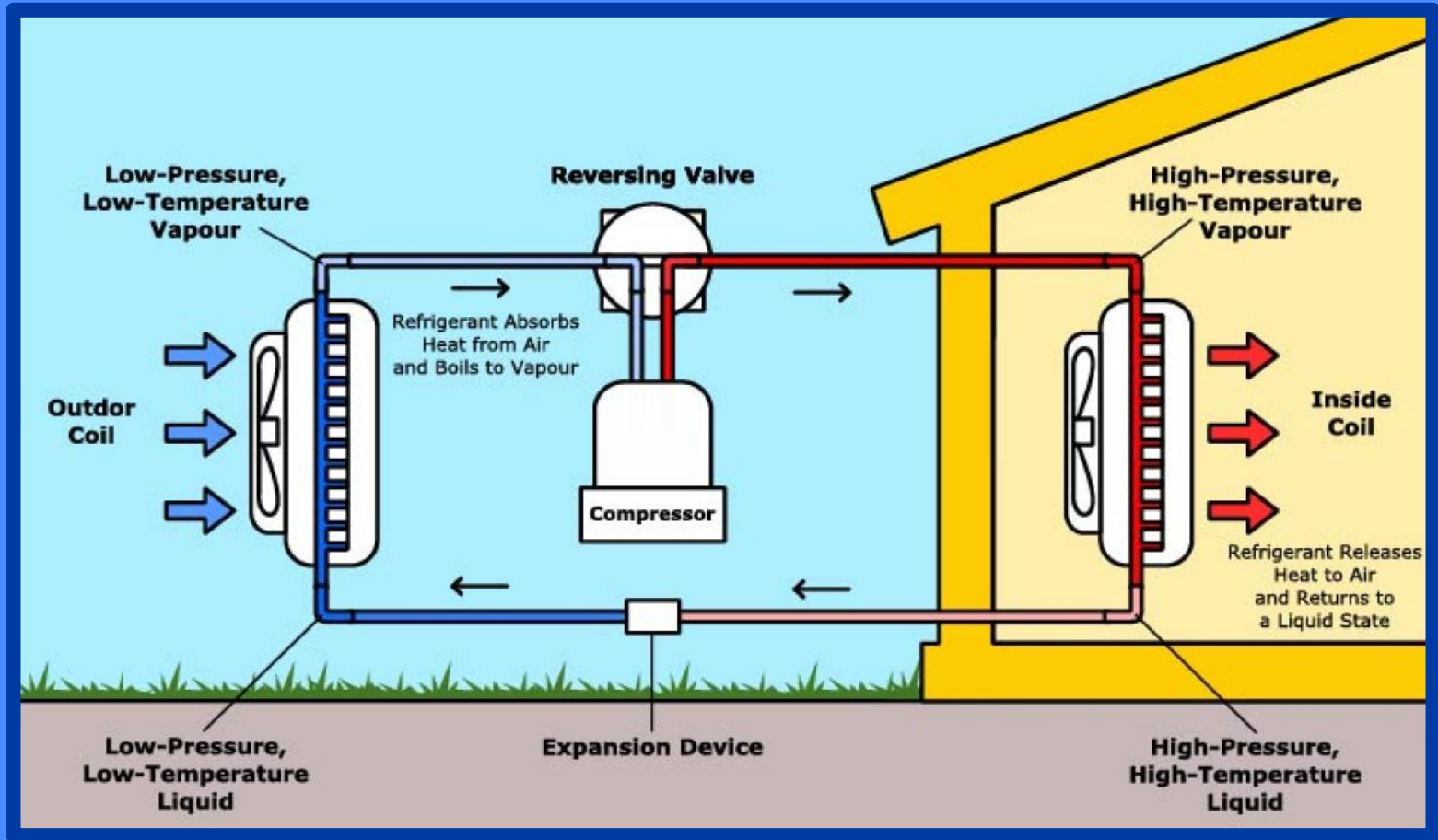
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01 Overview



To promote wider adoption of cold climate **air-source heat pumps**, we integrated **high-power pulse** technology to enhance the **overall efficiency** of ASHPs.

Pulse Electric Thermo Deicing (PETD)

An array of patented methods that use **high-power electric pulses** to **remove** ice, **prevent** ice formation, and either increase or decrease **ice-surface friction**.

Patent Inventors

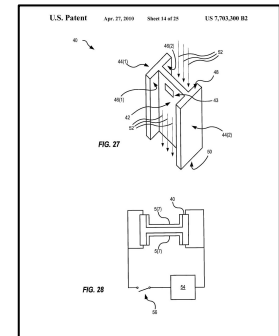
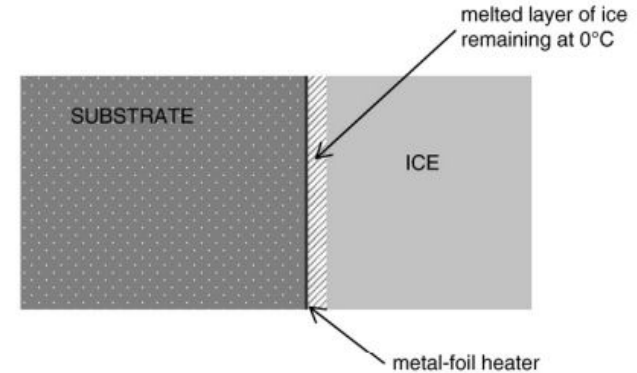
- Victor F. **Petrenko**: Dartmouth Engineering Professor
- Fedor V. Petrenko: Developed analytics for Dartmouth's Energy Initiative
- Cheng Chen: Dartmouth Alum, Former Ice Lab Researcher
- John **Chen** (Owner): Project Advisor, Former Ice Lab Researcher

Ice Theory and PETD

Ice's stickiness is due to its charged surface, which induces an opposite charge on the surface it adheres to.

PETD melts the interfacial ice layer, creating a thin film of water, and causing the ice to fall with the help of gravity.

Many applications: Deicing airplanes, power lines, windshields, ships, cars, trucks, offshore wind structures, roads, bridges, ski lifts, roofs, freezers, and more.



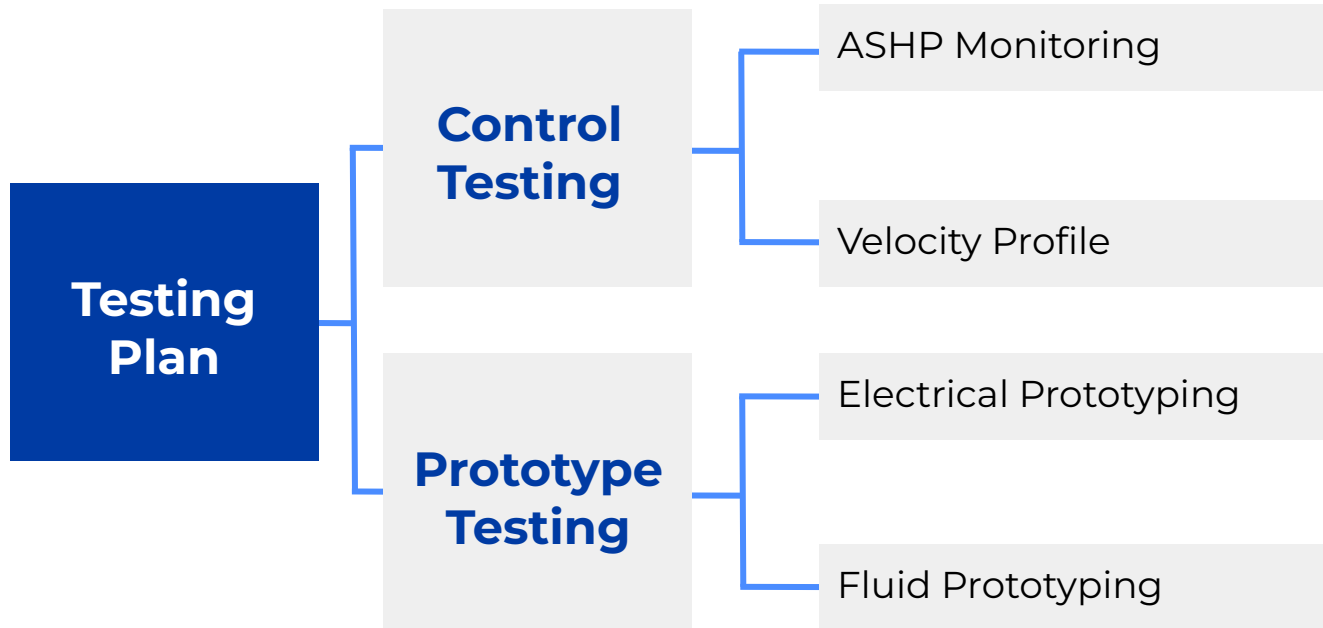
Specifications	Justification	Quantification
Efficient	Current market leading cold weather ASHPs are inefficient at below freezing temperatures	Coefficient of Performance (CoP) and energy (kW) of defrost cycle
Safe	Exposure to elements, animals, and homeowners	Acceptably low exposed voltage, isolated high voltage
Durable	Replacements are costly, and areas may have limited access to maintenance and repair	Thermal, environmental and corrosion testing
Affordable	Encourage homeowners in cold climates to install new ASHPs	Production and installation cost estimation
Legal	Compliance with electrical and refrigerant laws	Local Laws and EPA Regulations
Quiet	Comfortable audible sound level	Decibels (Db) and Location

Sponsor Goals

Our sponsor's long term goal is to **develop the integration of ASHP and PETD** technology for widespread, **global adoption**.

His vision for our group is to make that possible through a **prototype iteration, experimental procedure, data collection, and analysis**.

Testing Approach





02

Methodology Approach: Control Testing

ASHP Installation

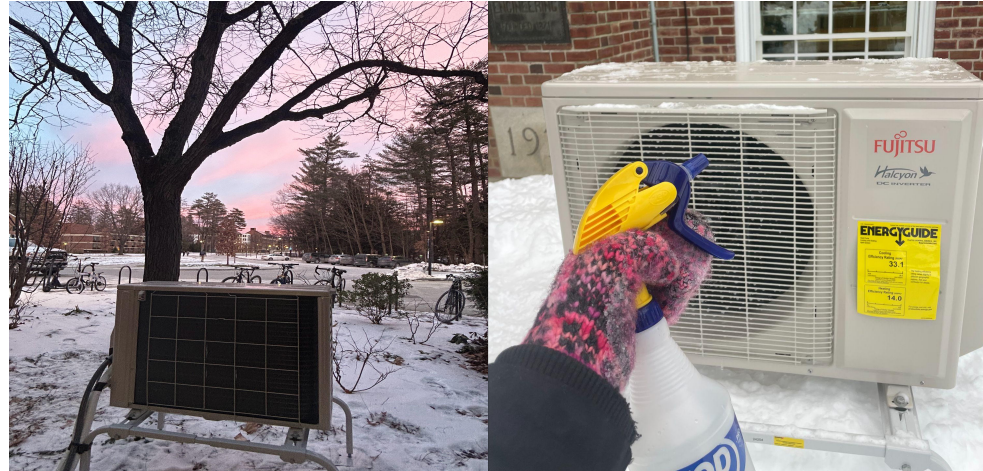
Indoor Unit

**Mitsubishi Hyper Heat
Model ASUG09LZBS**



Outdoor Unit

**Mitsubishi Hyper Heat
Model AOUG09LZAH1**



(Thank you Dave,
John, and Raina!)

Data Collection

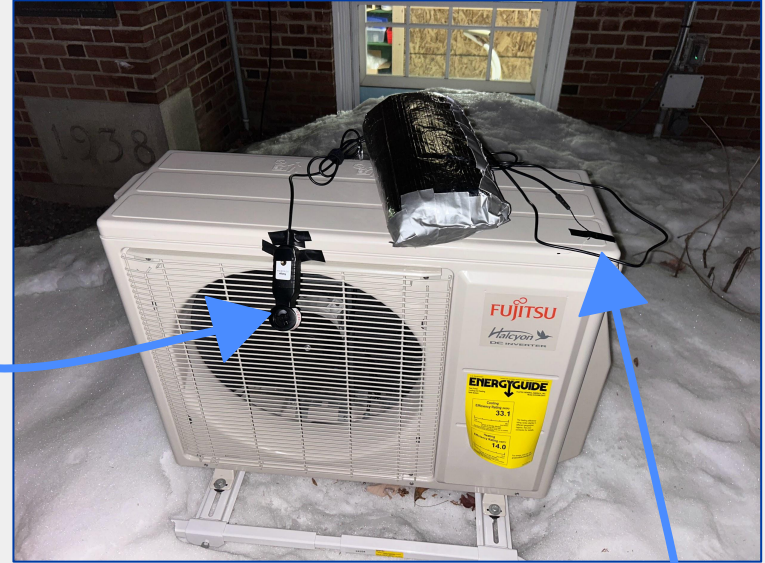
Sensor	Desired Parameter
Impeller Anemometer (2x)	Inlet and Outlet Airflow on Outdoor and Indoor Units
Exposed Thermistor (4x)	Direct Inlet and Outlet Temperature on Indoor and Outdoor Units Indoor and Outdoor Ambient Temperature (75 cm away)
Relative Humidity Sensor (1x)	Humidity at the outdoor unit inlet
Eyedro Home Energy Monitor	Monitors the kW that the ASHP pulls

Outdoor Unit (ODU)

Outlet Temperature on
Outdoor Condenser Fins



Inlet Airflow on Outdoor Fan



Ambient Temperature
(75 cm from Inlet)



LabQuest 2 in Insulating Sleeve

Indoor Unit (AHU)



Anemomaster

Ambient temperature
(75 cm from outlet)



LabQuest



Outlet airflow and
temperature



Using a single point flow from the impeller anemometer is sufficient and accurate because we can account for the **velocity profile**



Velocity Profile

Velocity Profile Justification

- Recommendations from advising team
 - Alexa Freitas (Trane Technologies)
 - Cheng Chen (Thayer Ice Lab Researcher)
 - Raina White (Thayer Systems and Fluids)
- 1. Achieve uniform flow across outlet
- 2. Calculate velocity profile
- 3. Calculate CFM
- 4. Calculate COP

$$CoP = \frac{Q_{out}}{Q_{in}} = \frac{CFM \cdot \Delta T \cdot 1.08}{(kWh_{ODU} + kWh_{AHU}) \cdot 3413}$$

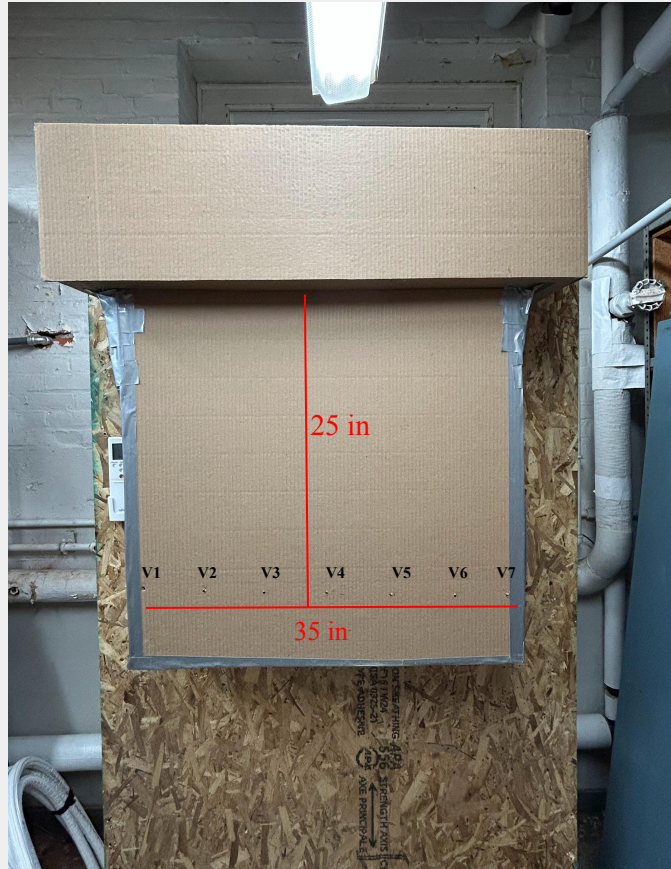
Anemomaster 6036
Professional HVAC
Anemometer
(Thank you Raina!)



1. Build Ductwork for Velocity Profile



2. Calculate Velocity Profile



$$V1 = 0.15 \text{ m/s}$$

$$V2 = 0.16 \text{ m/s}$$

$$V3 = 0.18 \text{ m/s}$$

$$V4 = 0.16 \text{ m/s}$$

$$V5 = 0.17 \text{ m/s}$$

$$V6 = 0.18 \text{ m/s}$$

$$V7 = 0.15 \text{ m/s}$$

$$\mathbf{V_{avg} = 0.1614 \text{ m/s}}$$

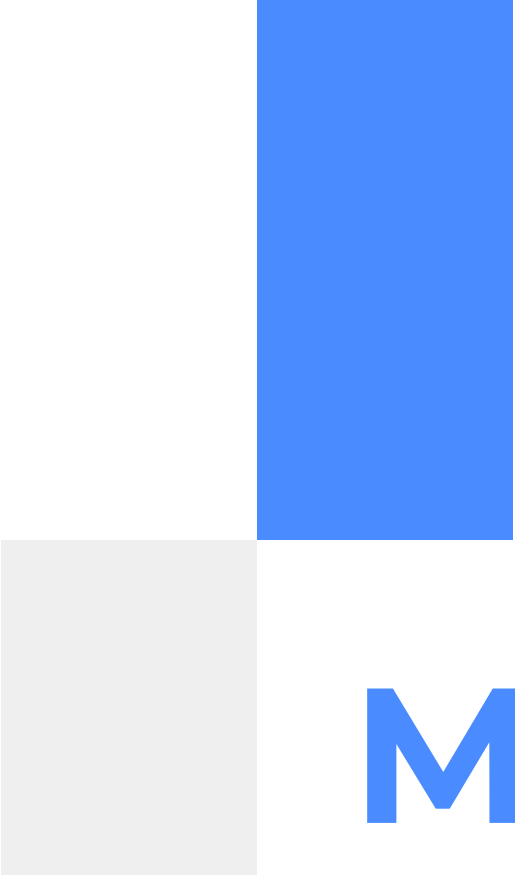
3. Calculate CFM

$$\text{Ductwork Volume} = 30 \times 37 \times 11 = 11210 \text{ in}^3 = 7.07 \text{ ft}^3$$

$$\text{CFM (cubic feet per minute)} = 224.61$$

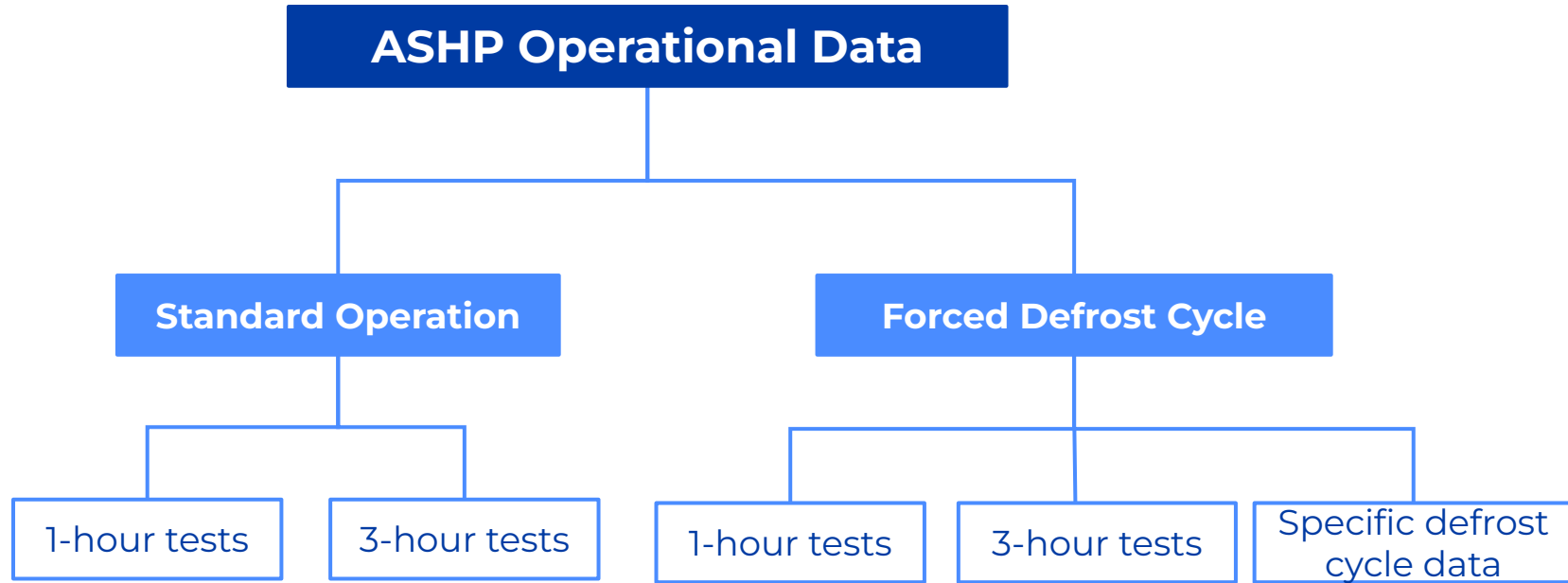
Higher CFM generally means
better performance and versatility

4. Calculate COP

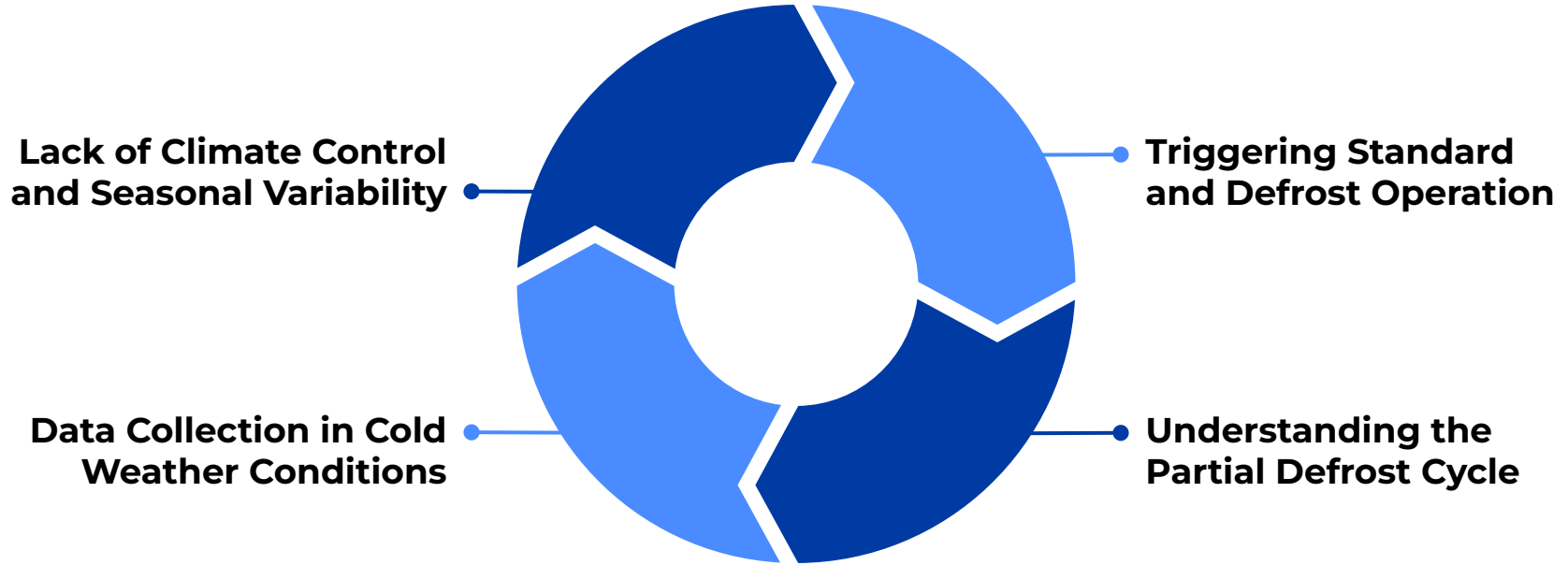


ASHP Monitoring

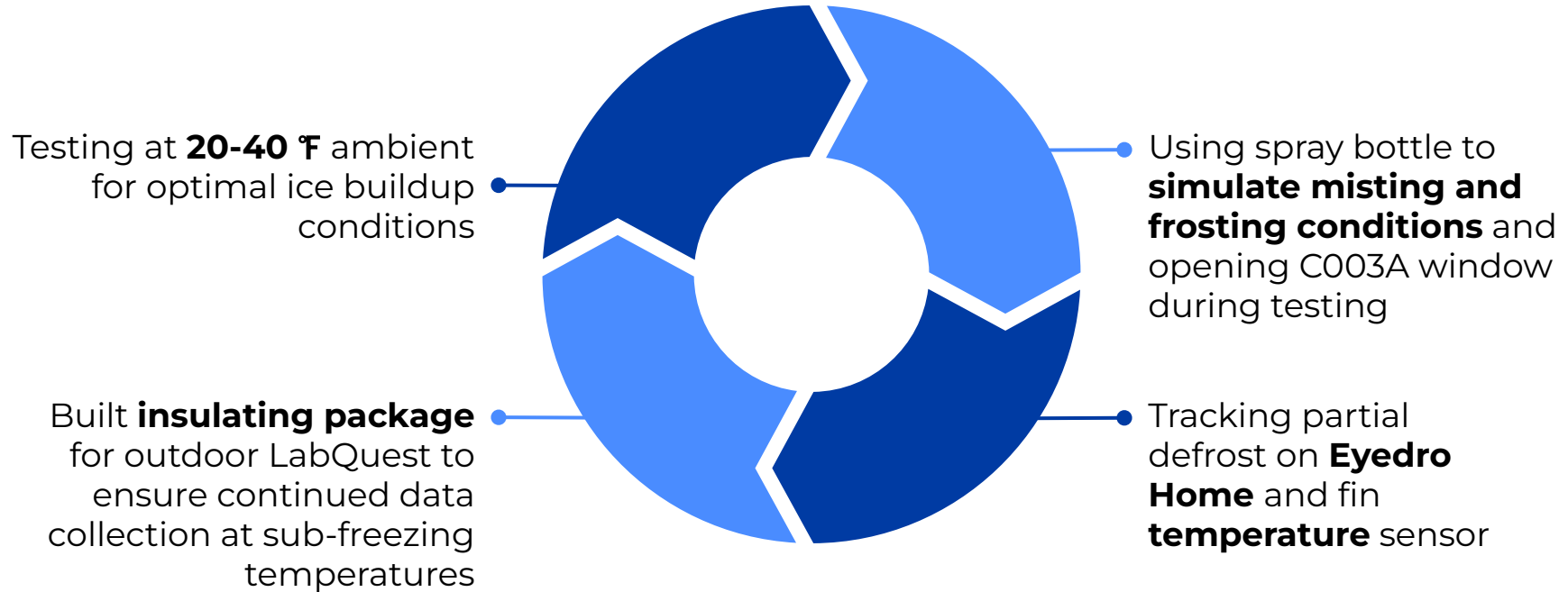
Goal: Gather Data on ASHP Operations



Challenges Faced

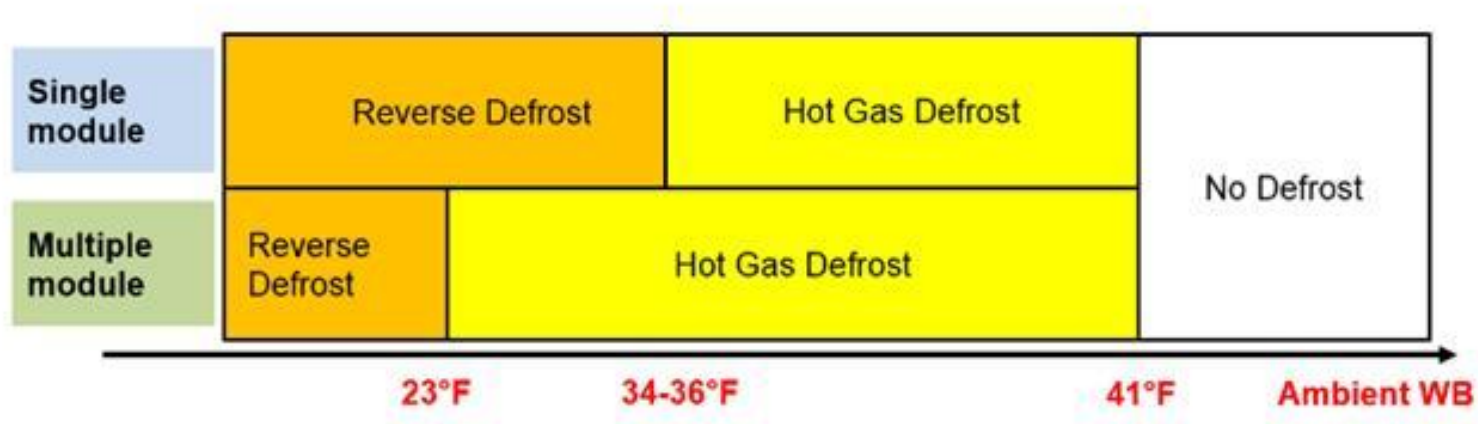


Solutions



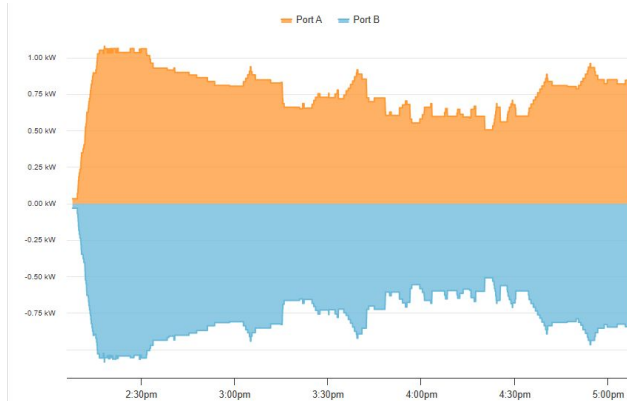
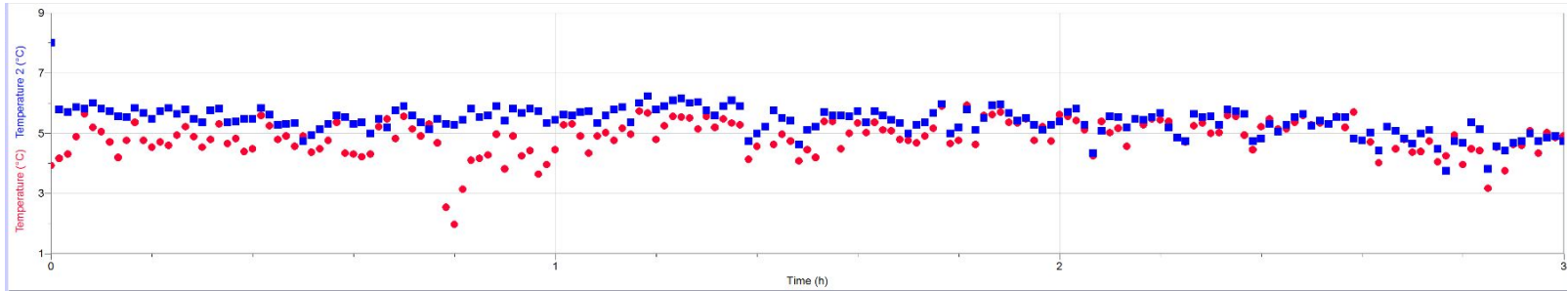
Full and Partial Defrost

- Full: **100%** of hot gas directed to ODU to defrost condenser fins
- Partial: **~50%** of hot gas directed to ODU, **~50%** used to heat AHU



Standard Operation Data

Outdoor Unit (3-Hour Test)

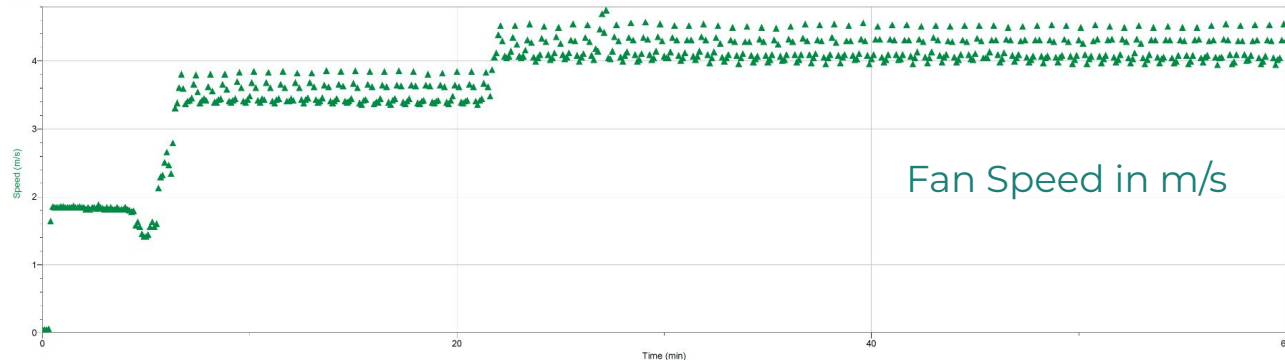
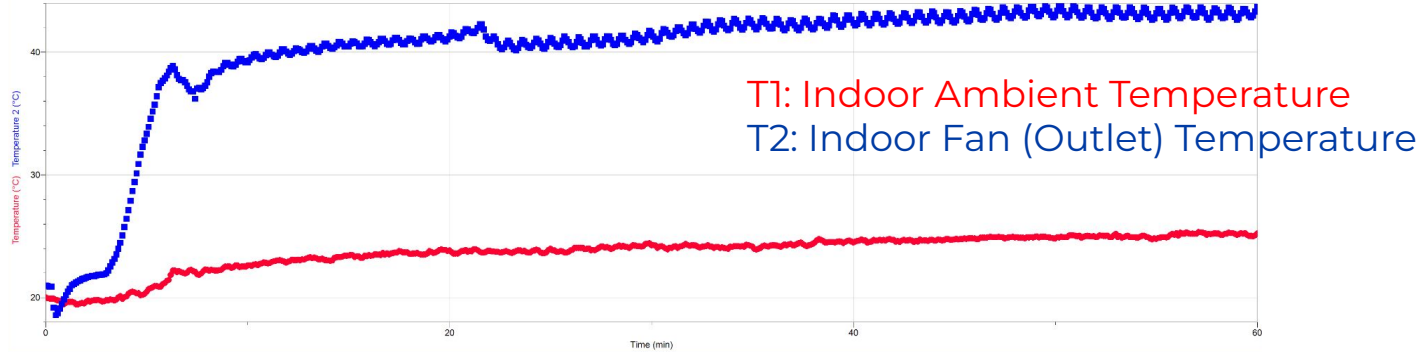


T1: Outdoor Fin (inlet) Temperature
T2: Outdoor Ambient Temperature

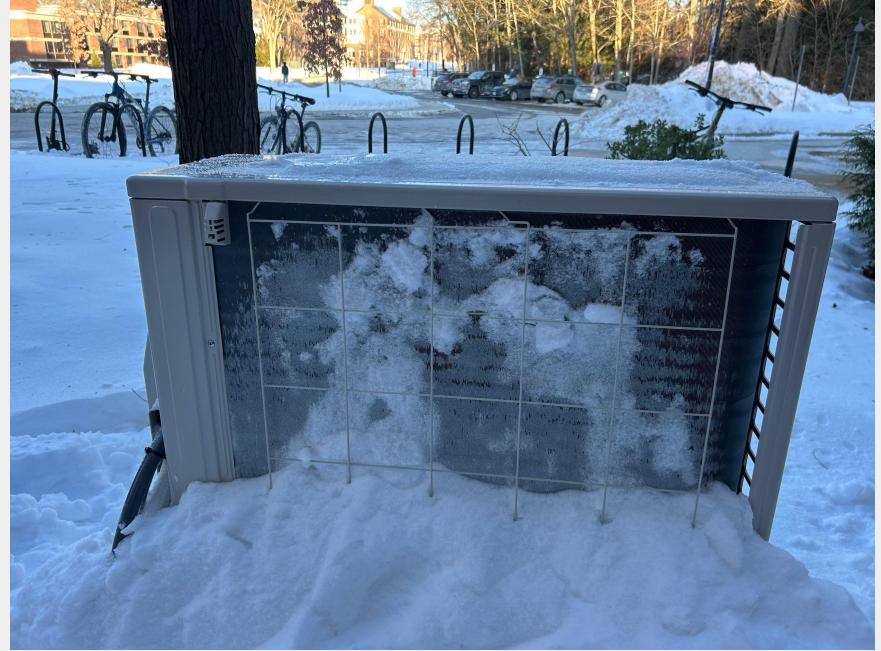
Port 1: Power Usage in kW
Port 2: Power Usage in kW

Standard Operation Data

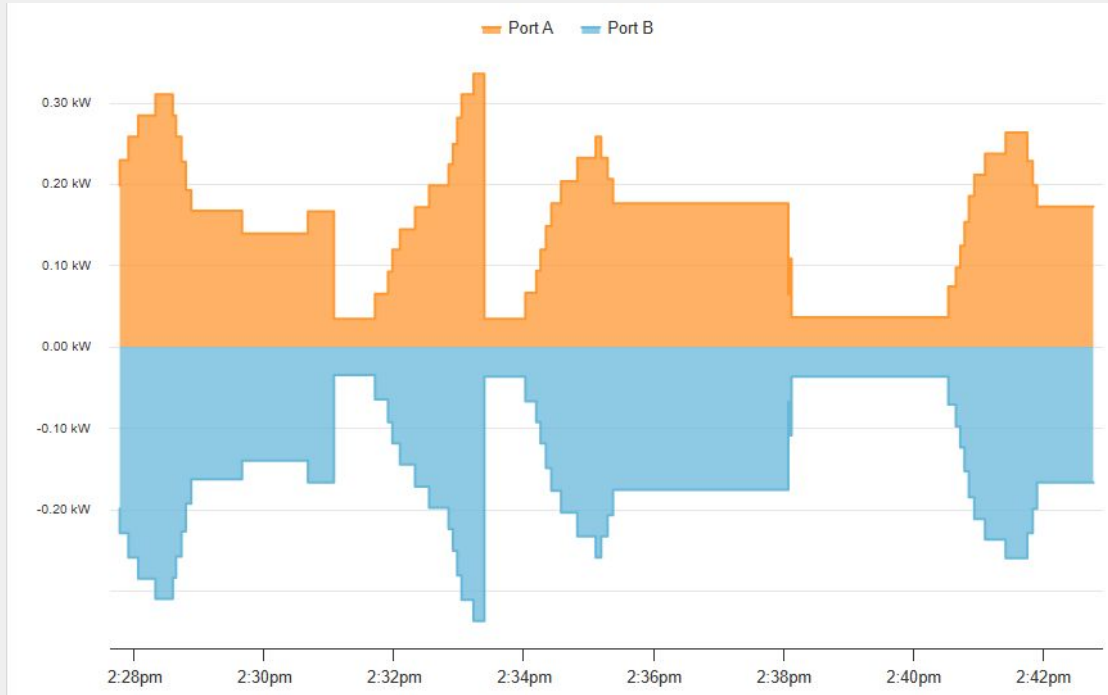
Indoor Unit (3-Hour Test)



Forced Defrost Cycles



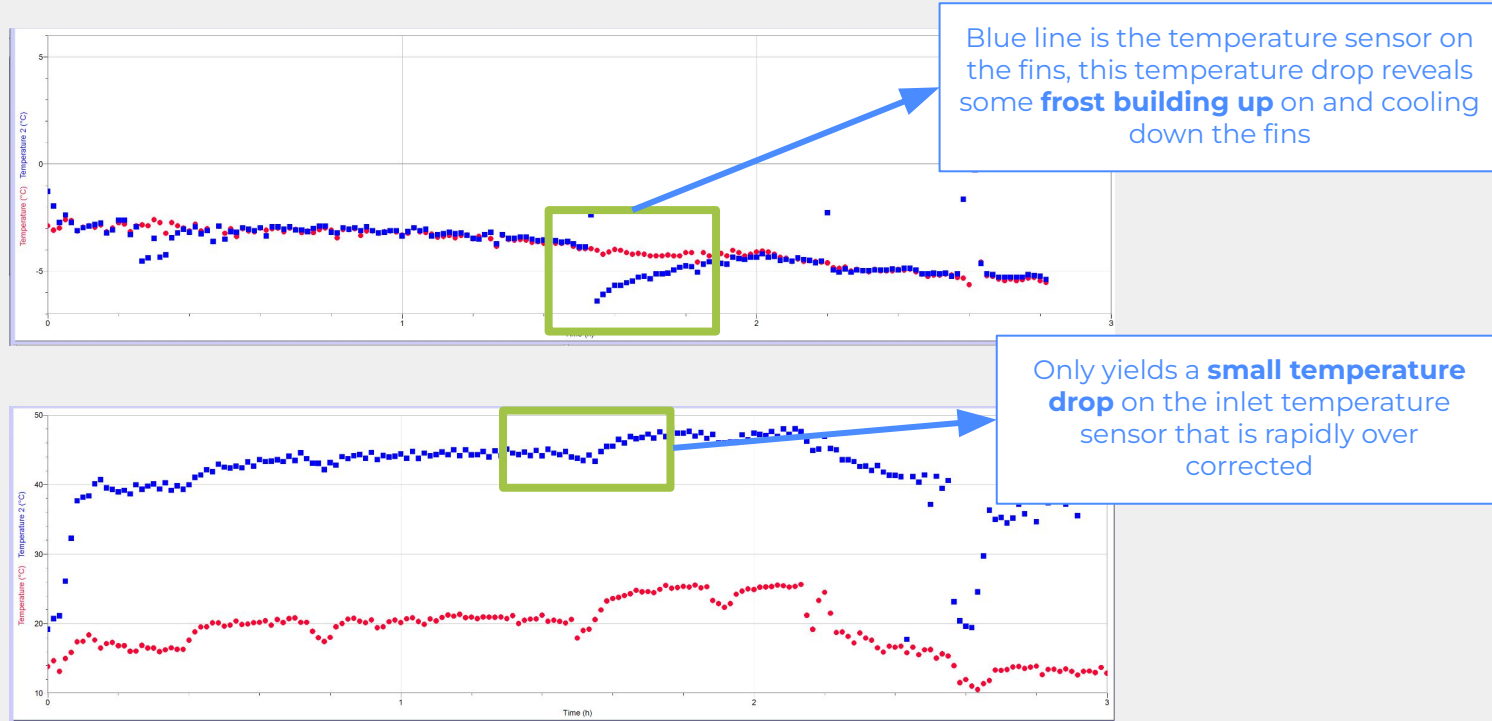
Full Defrost Cycle



Time: 9:05:04 mins

**Power Consumption:
~4.68 kW**

Partial Defrost Cycle



Only took ~**4:40 mins**
and used ~**2 kW** power



03

Methodology Approach: Prototype Testing

Parallel Design

Power Supply

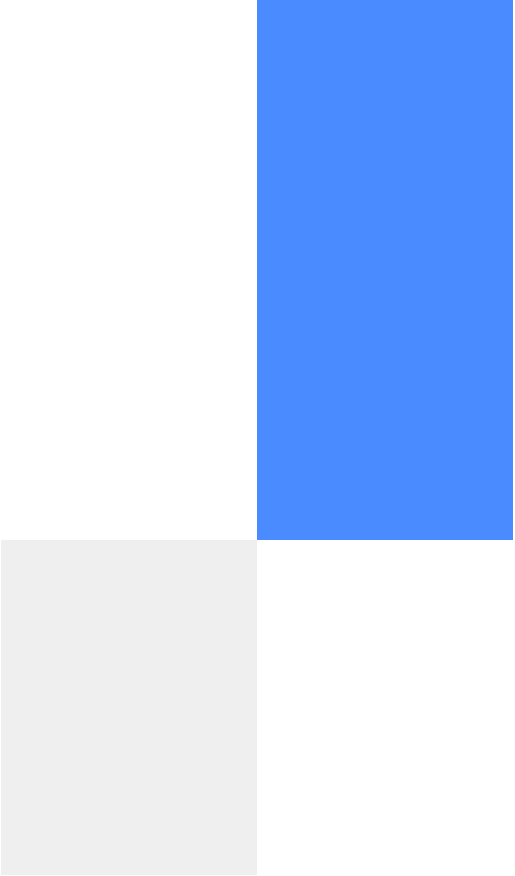
- ❑ Need ability to safely control 120/220V AC input to the coil
- ❑ Learn high power electronics

Icing Methods

- ❑ Need method of cooling coil so that it would freeze water vapor in the air

PETD Implementation

- ❑ Shifting focus to smaller scale testing
- ❑ Transformer specifications
- ❑ Increasing power capability



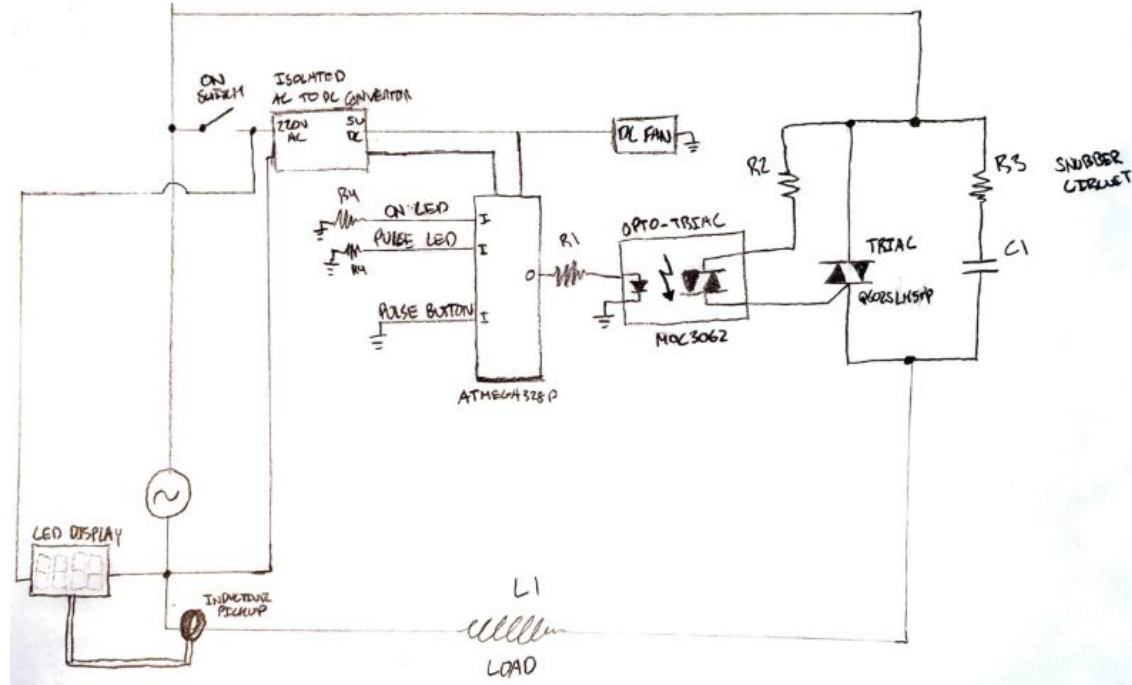
Power Supply

Power Supply - Schematic

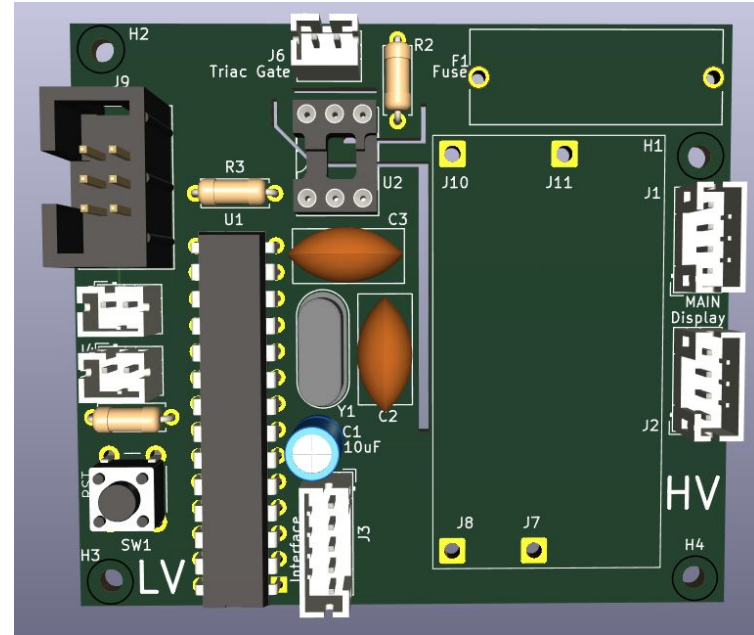
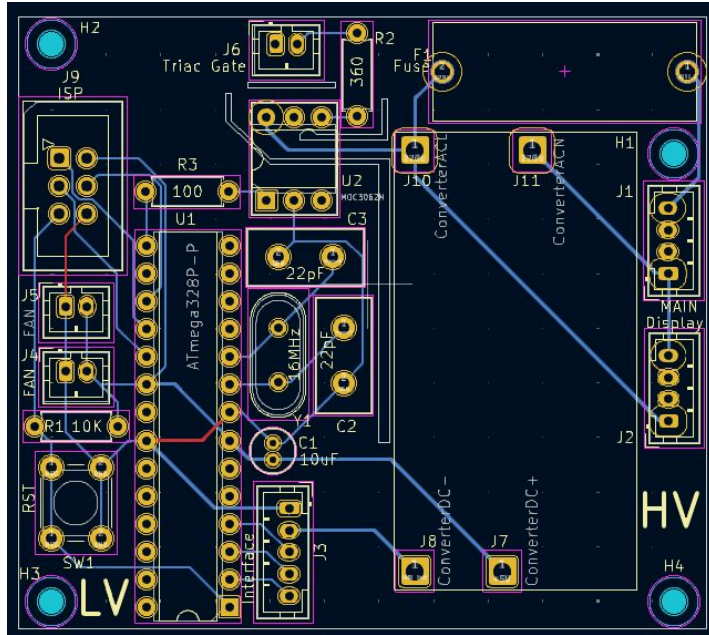
Basic Idea: Create a control system that toggles AC input

Design: Use a microcontroller (atmega328p) to operate an optocoupler (transfers electrical signals between isolated circuits) which will drive a triac (semiconductor switch). The output of the triac will go straight to the load, and allow for steady di/dt .

Safety: Certified isolated AC to DC converter, isolated LV and HV, 2A fuse, heatsink, waterproof housing



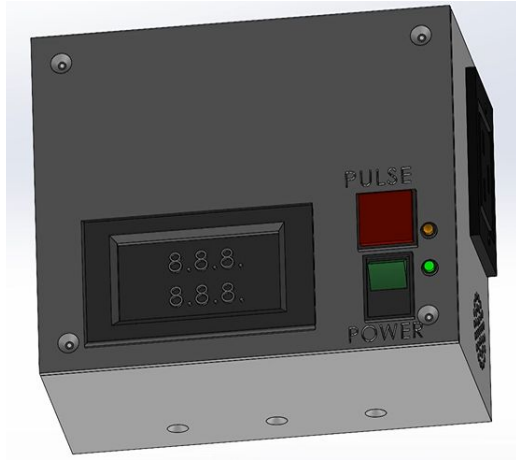
Power Supply - PCB



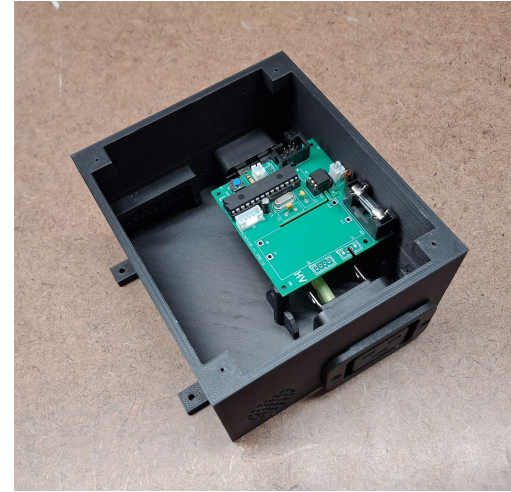
* This design follows IPC clearance and creepage guidelines for 240 AC mains.

Power Supply - Housing

Custom Design



Assembly



Power Supply - Isolated Variac

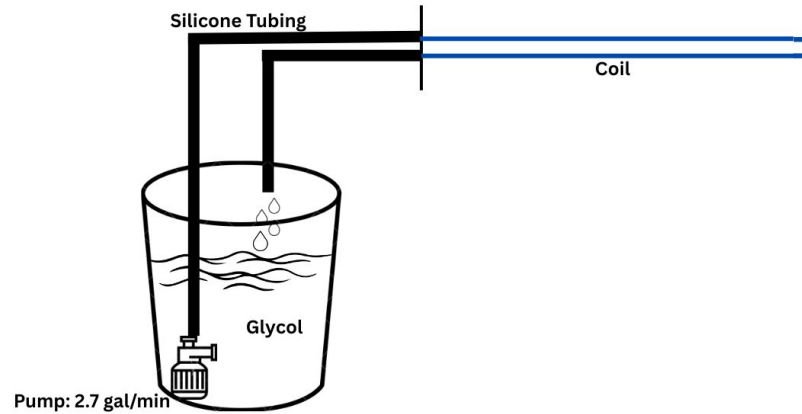
- Proven electrical isolation from mains supply to coil
- Manual switch — safety
- Simple voltage adjustments





Icing Methods

Icing Methods - Fluid Loop



Icing Methods - Fluid Loop Testing

Conducted a preliminary test to verify the possibility of freezing water vapor using this method. Ambient temperature was 30F.

Test #1: Antifreeze, ice, salt, coil, tubing, hose clamps, pump, and a misting bottle

- The coil itself was cold to the touch, but no ice was forming

Test #2: Added a box fan to the setup

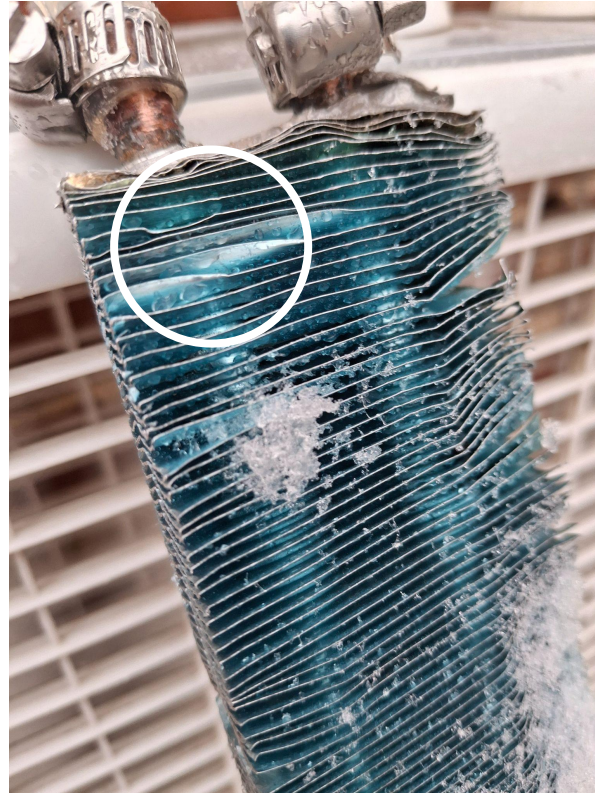
- Results! Water droplets began freezing

Test #3: Placed snow on coil

- Snow remained in position



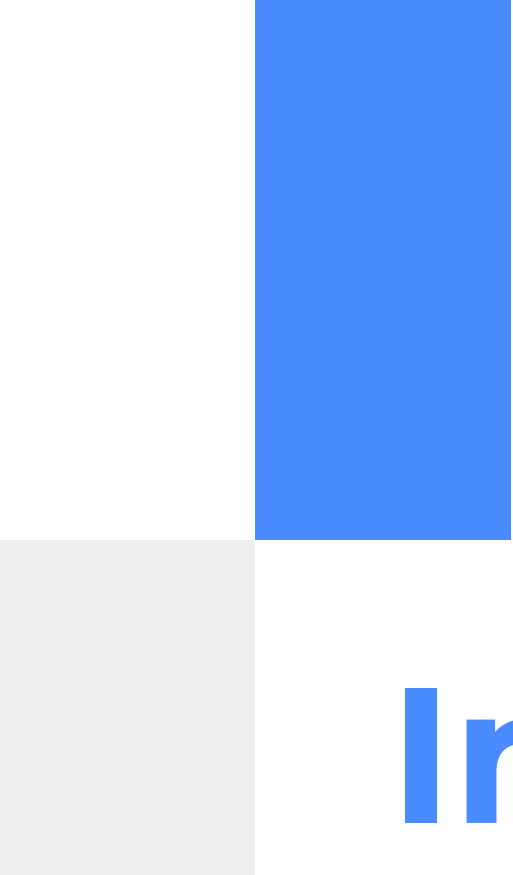
Icing Methods - Fluid Loop Testing



Icing Methods - Fan Tunnel



After our initial fluid loop test, we wanted to focus the airflow onto the coil to further **improve our icing capabilities**



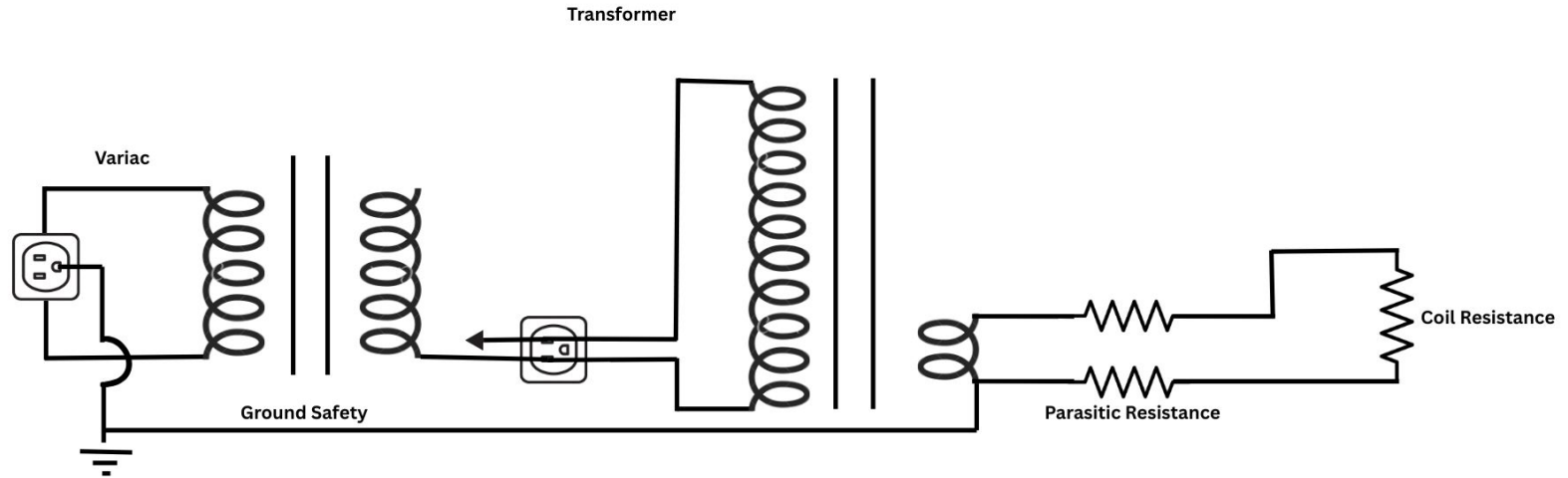
PETD Integration

Transformer Characterization

- Measuring inductance, resistance, real voltage transfer
 - Done with Bob Barry and Professor Sullivan
- Safety: electrical isolation not fully trusted
- Also concluded which leads to use



Electrical Design





Design Iterations

Cables + Solder

- Soldered 6 stranded 12 gauge wire to pipe
- Mechanically connected wires to transformer
- Limited to 120 A



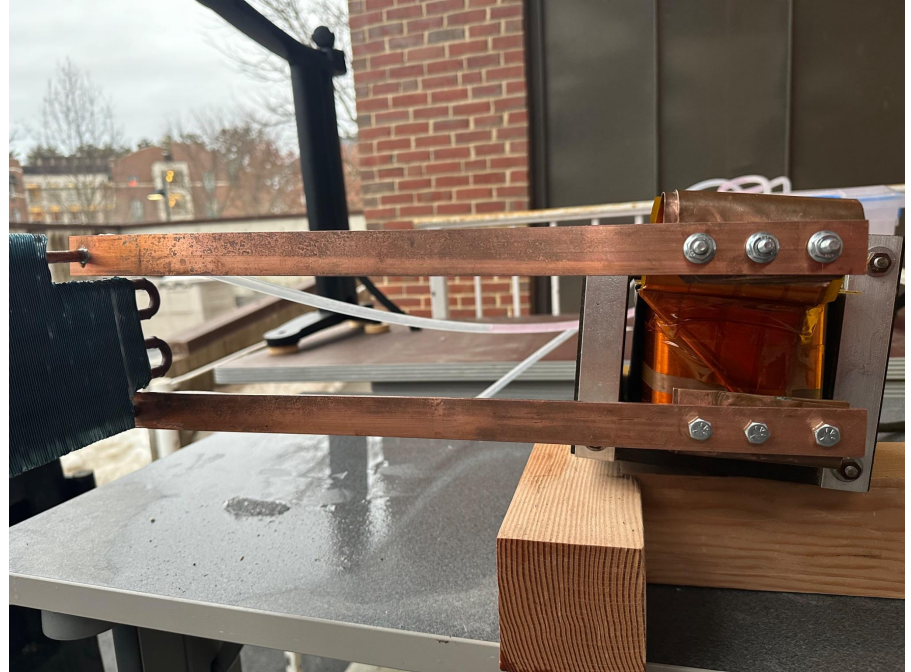
Cables + Bronze Busbars

- Mechanically screwed wire to busbars
- Mechanically connected and soldered busbars to pipe
- Mechanically connected wires to transformer
- Limited to 150 A

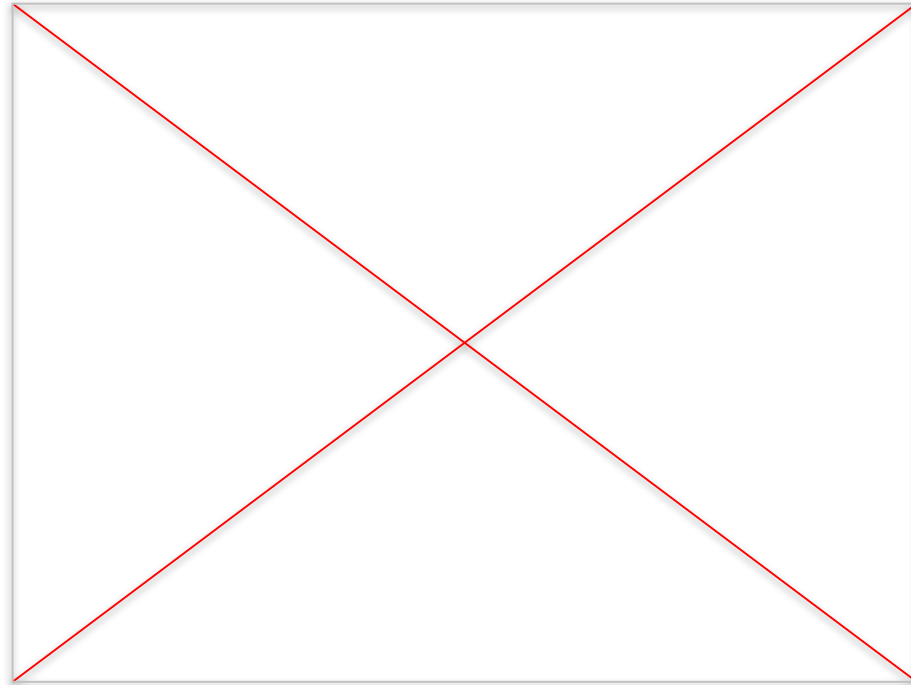
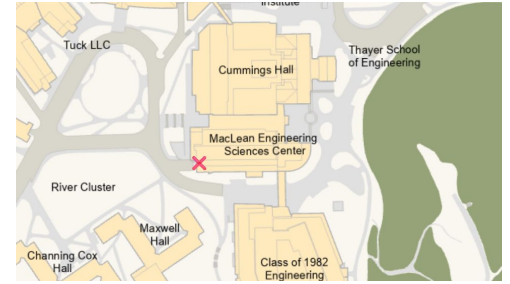


Copper Busbars

- Mechanically connected and soldered busbars to pipe
- Mechanically bolted busbars to transformer
- High current capability



Full Test Setup

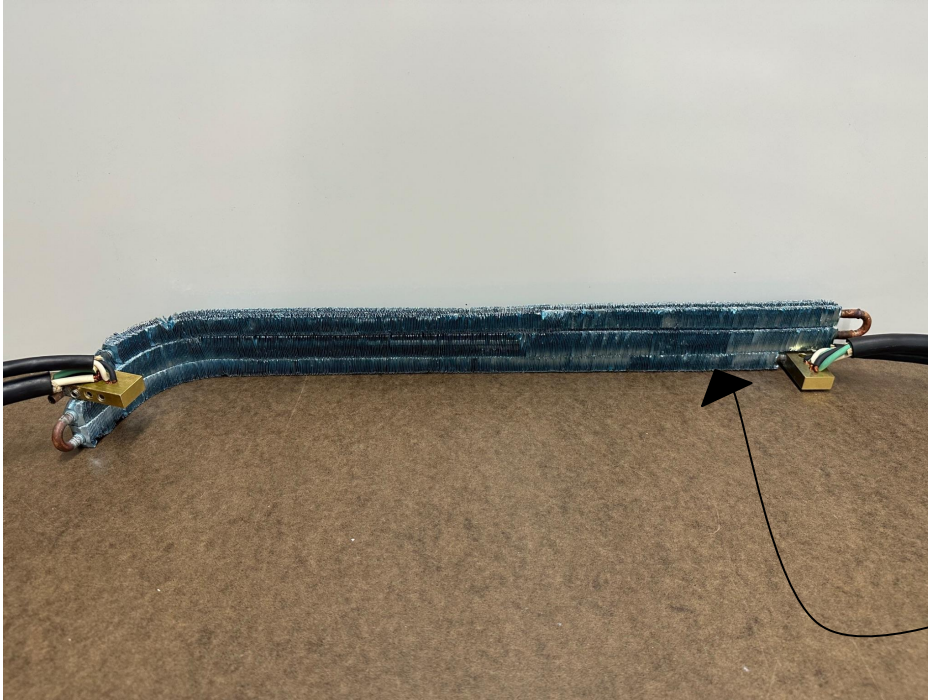


1 Length



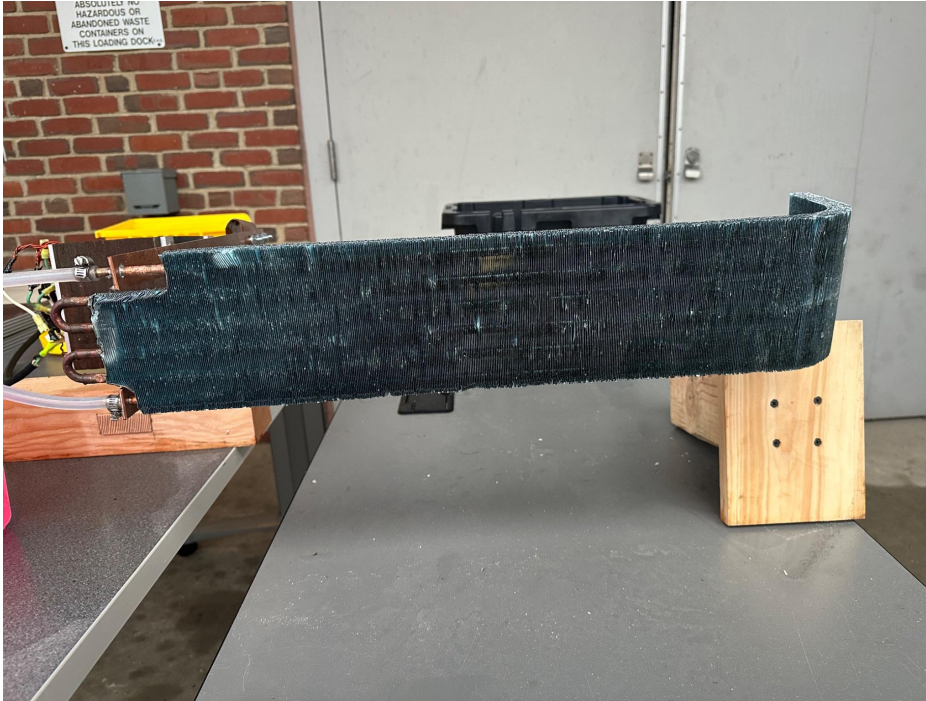
Custom built
stand with 3
printed holders

3 Lengths



Cuts made in
between pipes
led to uneven
deicing

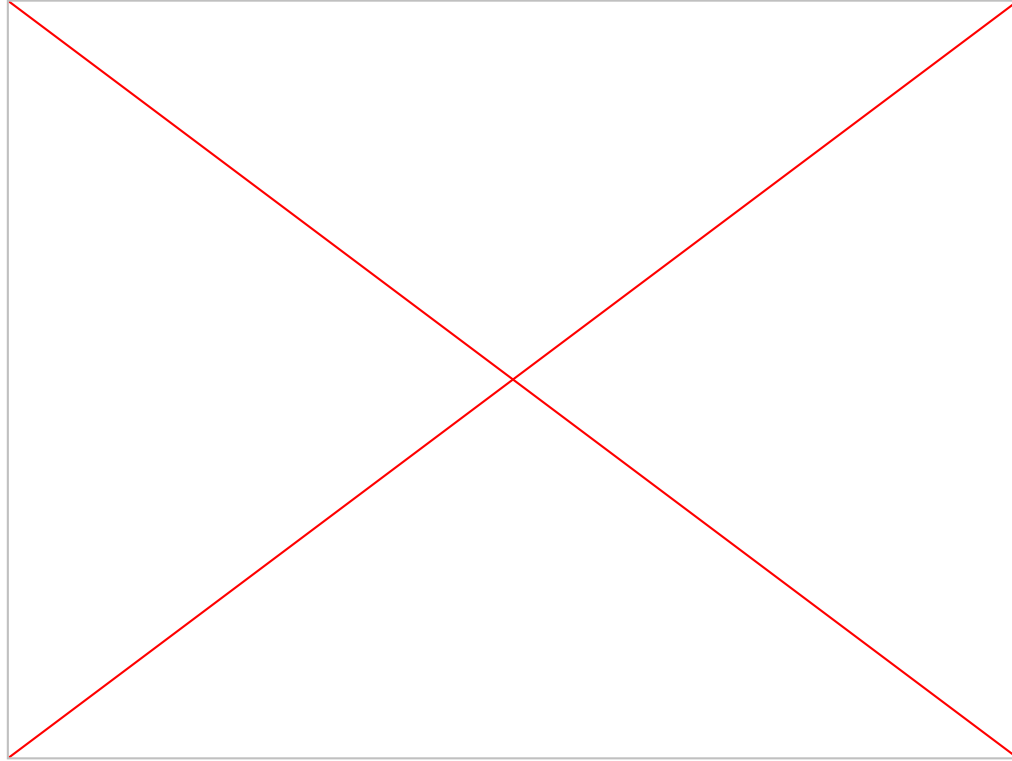
6 Lengths



One complete coil ensures uniform deicing

* LV prevents current from traveling through aluminum fins

Demo



Testing Results

1 Length

64.8 W → 3.6 kW

6 minutes

363 Wh

3 Lengths

~350 W → 6.5 kW

4:54 minutes

535 Wh

6 Lengths

~730 W → 6.8 kW

2:28 minutes

283 Wh

Takeaways

0.432 kWh

Average Total Power
Consumption
(extrapolated)

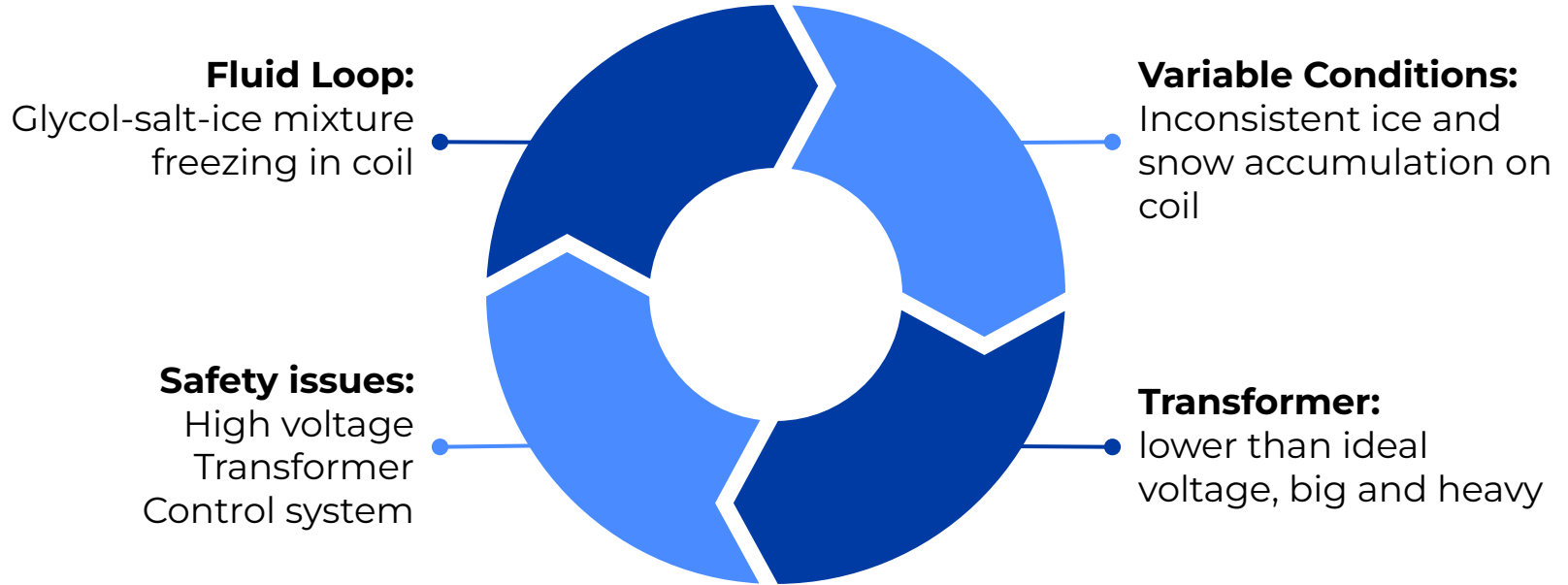
0.342 kWh

Average Power
Consumption Under
Favorable Conditions
(extrapolated)

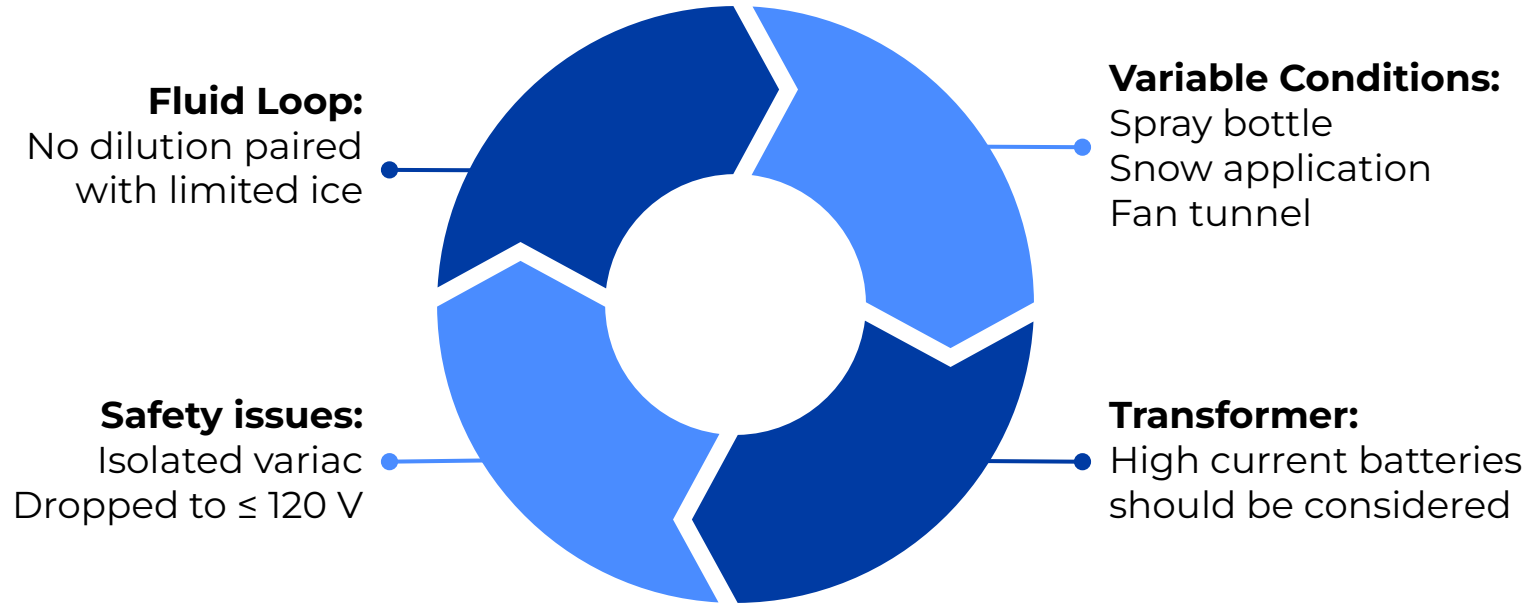
0.613 kWh

Average Power
Consumption Under
Unfavorable Conditions
(extrapolated)

Challenges Faced



Solutions





04 Deliverables: Results

CoP Calculation

Coefficient of Performance (**CoP**) quantifies efficiency of transfer of electricity input into heating or cooling output as an **instantaneous measurement**

$$CoP = \frac{Q_{out}}{Q_{in}} = \frac{CFM \cdot \Delta T \cdot 1.08}{(kWh_{ODU} + kWh_{AHU}) \cdot 3413}$$

$$CoP_{HP} = \frac{Q_H}{W_{in}}$$

CoP Calculations (Defrost Specific)

$$CoP = \frac{Q_{out}}{Q_{in}} = \frac{CFM \cdot \Delta T \cdot 1.08}{(kWh_{ODU} + kWh_{AHU}) \cdot 3413}$$

$$CFM = 224.61$$

$$\Delta T = 24 \text{ }^{\circ}\text{F}$$

$$kWh_{combined} = .702$$

$$CoP = \frac{224.61 \cdot 24 \cdot 1.08}{.702 \cdot 3413}$$

$$CoP = 2.43$$

CoP Comparisons

CoP Defrost

$$\text{CFM} = 224.61$$

$$\Delta T = 24\text{ }^{\circ}\text{F}$$

$$\text{kWh}_{\text{combined}} = 0.702\text{ kWh}$$

$$\text{CoP} = \frac{224.61 \cdot 24 \cdot 1.08}{.702 \cdot 3413}$$

$$\text{CoP} = 2.43$$

CoP Standard

$$\text{CFM} = 224.61$$

$$\Delta T = 24\text{ }^{\circ}\text{F}$$

$$\text{kWh}_{\text{combined}} = 0.150\text{ kWh}$$

$$\text{CoP} = \frac{224.61 \cdot 24 \cdot 1.08}{.150 \cdot 3413}$$

$$\text{CoP} = 11.37$$

Final Comparison

ASHP Defrost

$$4.68 \text{ kW} \cdot 0.150833 \text{ hr} =$$

0.702 kWh

Prototype

$$6.37 \text{ kW} \cdot 0.07 \text{ hr} =$$

0.432 kWh



05

Societal Impacts and Economic Analysis

Societal Impact

1 Political

Advanced, high-efficiency ASHPs designed for cold climates have the potential to influence policymakers to enact more supportive regulations and incentives for renewable energy adoption.

2 Environmental

Implemented safety measures to eliminate the risk of electrocution to local wildlife and prevent refrigerant leaks, safeguarding soil integrity and protecting plant life

3 Economical

ASHPs designed for greater efficiency in cold climates deliver substantial long-term economic advantages, such as sustained energy savings, reduced operational costs, and a stronger return on investment over their lifespan

Economic Analysis

Components	Cost		Ratings
Breaker	\$85.00	/unit	300 A 48 V
Relay	\$20.00	/unit	200 A 24 V
Transformer	\$100.00	/unit	24 V 200 A
Controller	\$15.00	/unit	
Wiring	\$5.00	/unit	
Expenses	Cost		
Additional Labor	\$15.00	/hour	
	\$45.00	/unit	
Revenue	Amount		
Additional price	\$500.00	/unit	
Added revenue	\$230.00	/unit	

Market Adoption

Our sponsor's goal is to have convincing data to pitch to **HVAC manufacturers**.

Our project did not provide entirely conclusive results, however it justifies further data collection.

If results are more certain, this product could save energy on a global scale.



06

Conclusions and Future Work

Conclusions

- Proved significant drop in CoP during defrost cycle
 - Added potential **novel contribution** to literature on defrost cycle
- PETD uses less energy than classical defrost cycle
 - Difference is **not as substantial** as hoped
 - May not be worth the cost
- Variable conditions and inconsistent data for both control and prototype testing contribute to higher uncertainty
 - Better **controlled lab** needed to do full cost benefit analysis

Next Steps

Further prototype testing

- Scale up to a full size system
- Weigh coil, frost, collected frost
- Vibration to remove water

Re-evaluate power supply

- Consider using 30V
- Still safe
- Less current requirement
- Smaller, lighter

Improve rigor of defrost cycle testing

- Use Ice Lab facility
- Control temperature, humidity, etc.
- Repeatable conditions
- HVAC/Ice Lab Researchers

Special Thanks

Bob Barry

Cheng Chen

John Chen

Danny DeNauw

Sol Diamond

Alexa Freitas

Chris Magoon

Dave McDevitt

Emily Monroe

John Stark

Jason Stauth

Charlie Sullivan

Raina White



Thank You

Questions?

Appendix

Transformer Data

Inductance Secondary (mH) (Sullivan)	Inductance Secondary (mH) (Bob)	Primary Wires	Inductance Primary (mH) (Sullivan)	Inductance Primary (mH) (Bob)	DC Resistance Primary (Ohm) (Bob)	Turns Ratio (Sullivan)	Turns Ratio (Bob)	Turns Ratio (avg)	Vout Predicted (10V, 60 Hz, input)	Vout Real (10V, 60 Hz input)	Vout Real (10V, 100 kHz input)	Ratio (real/expected)
0.046	0.047	1->2	28	30.5	0.12	0.04053217417	0.03925536405	0.03989376911	0.3989376911	0.206		0.5163713648
		1->3		40.1			0.03423550533	0.03423550533	0.3423550533	0.197		0.5754260032
		1->4		50.68			0.0304530381	0.0304530381	0.304530381	0.187		0.6140602438
		1->5		61.04			0.02774863769	0.02774863769	0.2774863769	0.177		0.6378691522
		1->6		75			0.02503331114	0.02503331114	0.2503331114	0.166	0.195	0.6631164334
		2->3	0.429	0.43	0.02	0.3274539773	0.3306090222	0.3290314997	3.290314997	0.0453		0.01376767879
		2->4		1.754			0.1636945176	0.1636945176	1.636945176	0.134		0.08185979711
		2->5		3.731			0.1122370658	0.1122370658	1.122370658	0.2		0.1781942521
		2->6								0.244		
		3->4	0.429	0.43	0.02	0.3274539773	0.3306090222	0.3290314997	3.290314997	0.0455		0.01382846324
		3->5		1.57			0.1730211135	0.1730211135	1.730211135	0.124		0.07166755401
		3->6								0.206		
		4->5	0.33	0.34	0.01	0.3733549777	0.3718000728	0.3725775253	3.725775253	0.0375		0.01006501935
		4->6								0.134		
		5->6	0.529	0.535	0.03	0.2948839123	0.296395795	0.2956398537	2.956398537	0.055		0.01860371642

Prototype Data

	Voltage (V)	Amperage (A)	Power Test (W)	Avg Power (W)	Power Total (W)	Time (minutes)	Avg Time (mins)	Energy (kJ)	Energy (kWh)	Avg Energy (kWh)	Temp Coil Start (°F)	Temp Coil End (°F)
1 length	0.4	162	64.8	64.8	3628.8	6	6	1306.368	0.36288	0.36288	NA	NA
3 lengths	1.57	205	321.85	354.554	6007.866667	4.75	4.9	1712.242	0.4756227778	0.5352898444	28.5	NA
	1.6	206	329.6		6152.533333	6.25		2307.2	0.6408888889		28.2	100
	1.71	227	388.17		7245.84	3		1304.2512	0.362292		23	145
	1.71	215	367.65		6862.8	5.5		2264.724	0.62909		24.8	145
	1.7	215	365.5		6822.666667	5		2046.8	0.5685555556		23.8	185
6 lengths	3.41	220	750.2	736.6833333	7001.866667	2	2.4721	840.224	0.2333955556	0.2828640995	33	91
	3.4	215	731		6822.666667	3.333		1364.39688	0.3789991333		33	115
	3.39	215	728.85		6802.6	2.0833		850.3113948	0.2361976097		33	110
Averages					6371.96	4.212922222		1555.168608	0.4319912801			
Good Conditions					6251.606667	3.527716667		1229.632246	0.3415645127			
Bad Conditions					6612.666667	5.583333333		2206.241333	0.6128448148			

Major Setbacks

Fluid Loop

- Freezing
- Fluid velocity
- Glycol mixture

Safety

- High voltage
- Time intensive prototyping
- Control system

Transformer

- Lower than ideal voltage
- Big and heavy

Intro - 2
Control - 5
Prototype - 5.5
Combined - 1
Ending - 1

Electrical Design

Cables + Solder

Limited to 120 A

Simplest to fabricate,
but time intensive

Cables + Busbars

Limited to 150 A

Easiest to assemble for
testing

Busbars

Very high current

Hardest to transport

